AL-FARABI KAZAKH NATIONAL UNIVERSITY DEPARTMENT OF MECHANICS AND MATHEMATICS DEPARTMENT OF MECHANICS



Study of migration of radioactive elements in clay layers during the burial of radioactive waste

Prepared by Zhumanova M.I. Scientific adviser Tungatarova M.S.

A second shipment of low enriched uranium was delivered to our country

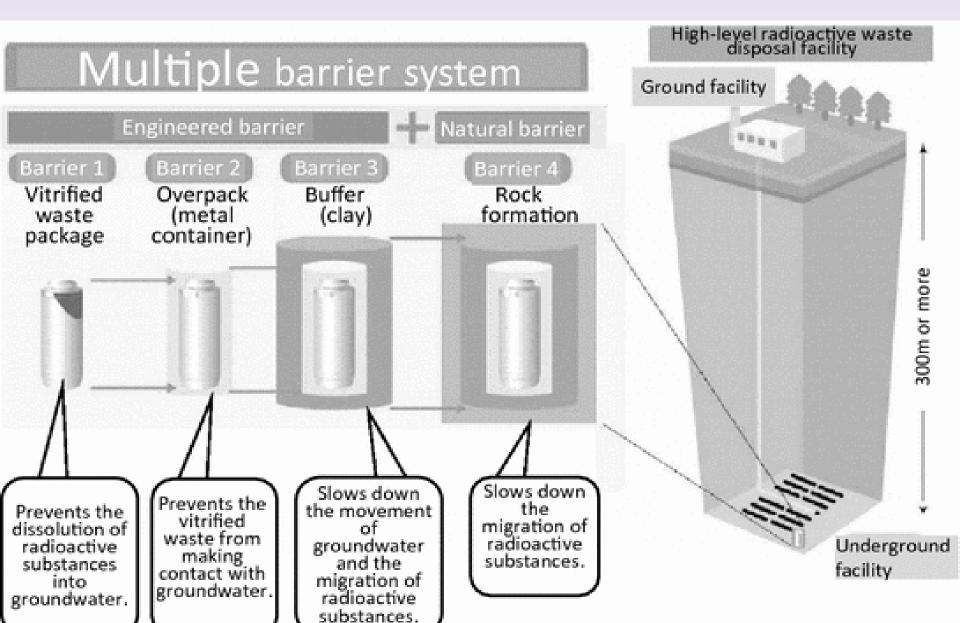




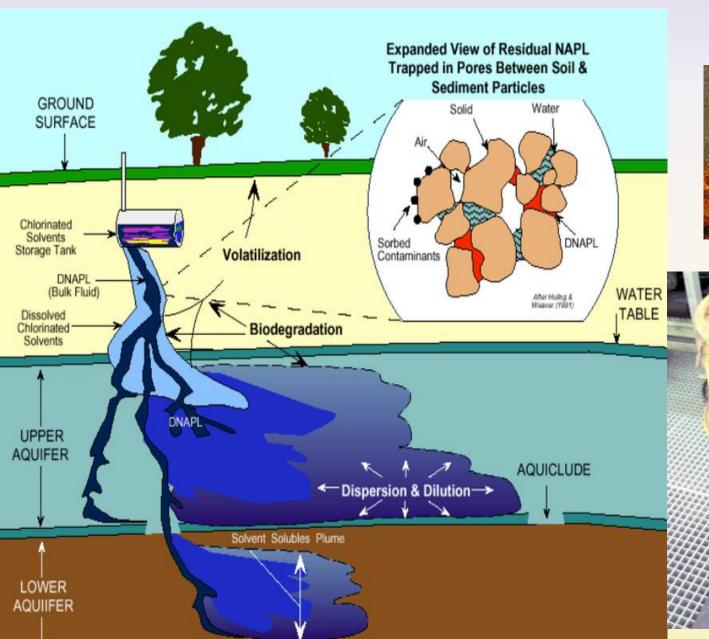




Near zone



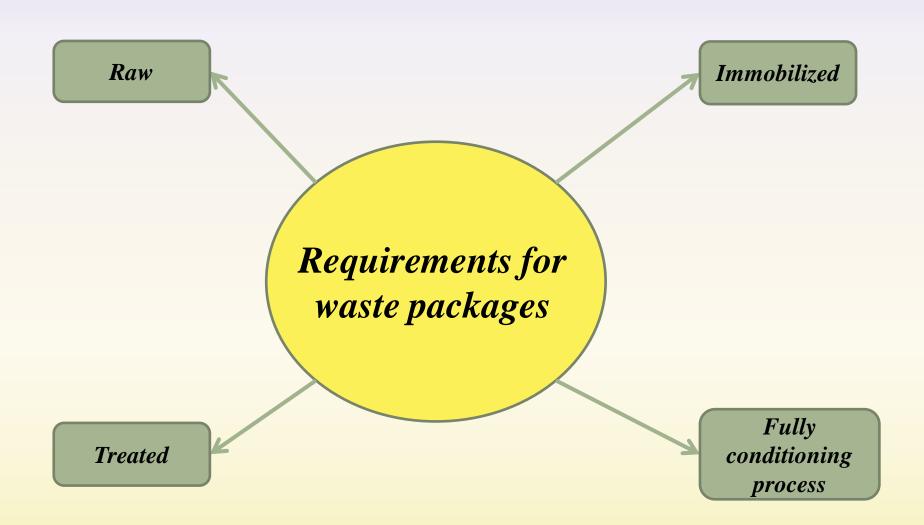
CORROSION OF PACKAGES WITH RADIOACTIVE WASTE







Radioactive waste may exist in several forms when it passes through the treatment and conditioning processes



Waste form, container and waste package

Waste form

Immobilization of waste

Conversion of waste into a waste form by

Solidification

Embedding or Encapsulation

Non-immobilized solid waste

Immobilized waste

Waste package

Waste form

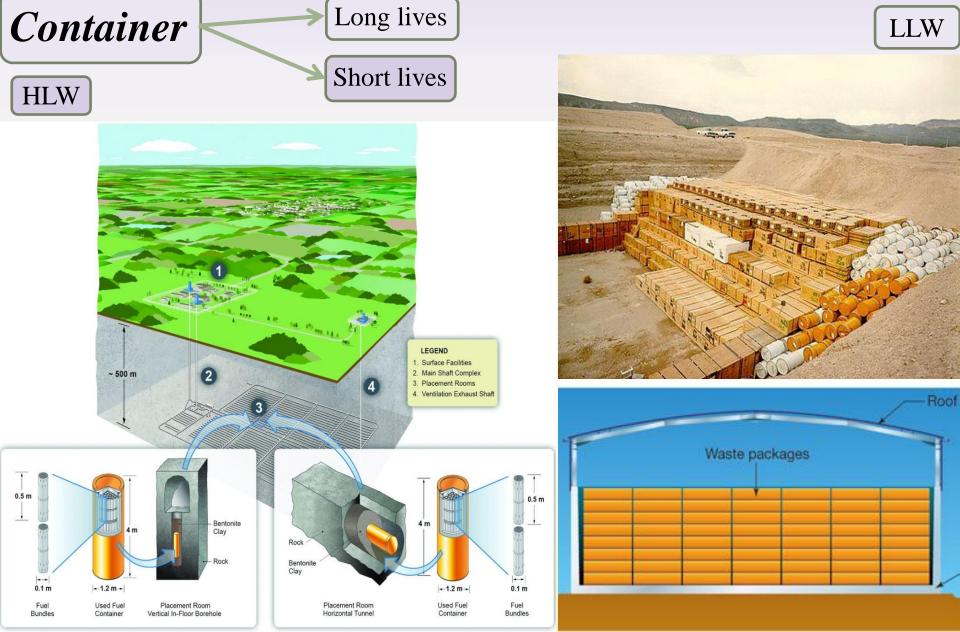
Containers

Internal barriers





Waste form, container and waste package



THERMAL EFFECTS

Temperature distribution factors

Type and age of waste

Dimensions and location of waste containers

Volume and properties of buffer materials and backfill materials

Storage design

Type of surrounding breed

THE GROUNDWATER

Changes in the physical properties of hard rock

Creation of low permeability barriers

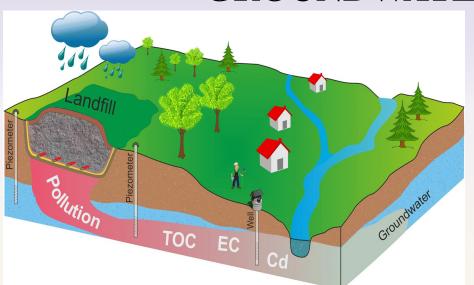
Drainage effect of underground excavation works

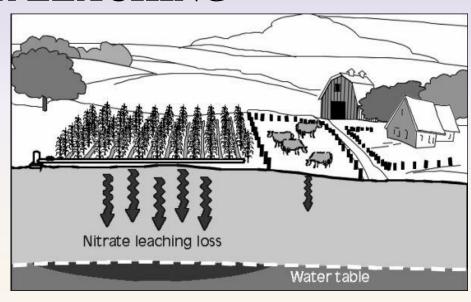
Heating due to the heat generated by radioactive waste

Movement of groundwater in the near zone

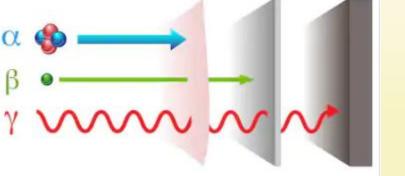
Each high-level waste (or spent fuel) disposal canister produces $\sim 1000-2000~\mathrm{W}$ of heat by decay processes. The maximum temperature in the bentonite buffer is reached at an early phase of the repository lifetime, after $\sim 50~\mathrm{y}$.

GROUNDWATER LEACHING









A change in the shape of the waste

A change in the composition of any liquid washing the waste

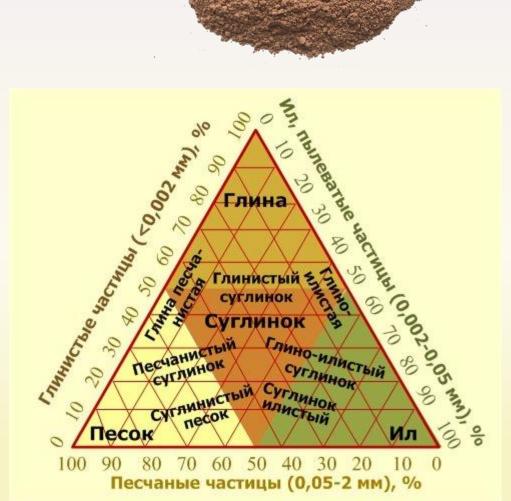
A change in the surrounding rock

RADIATION EFFECTS

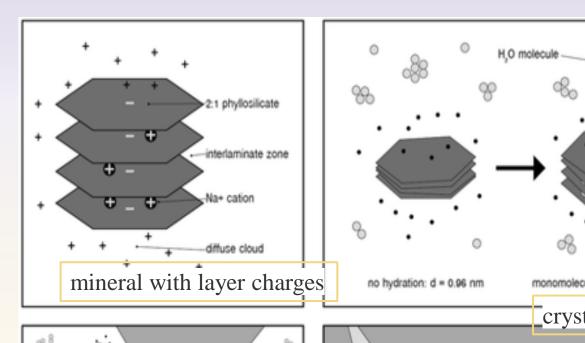
WATERPROOFING WITH CLAY

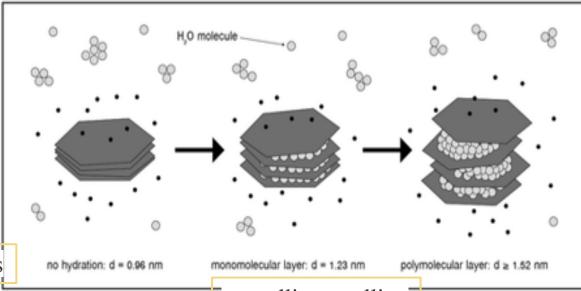
Ability to adsorb

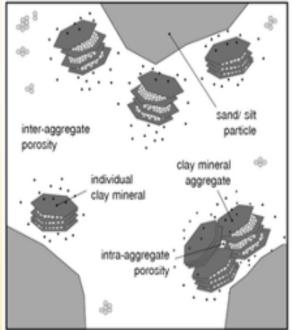
Exchange cations such as sodium or calcium

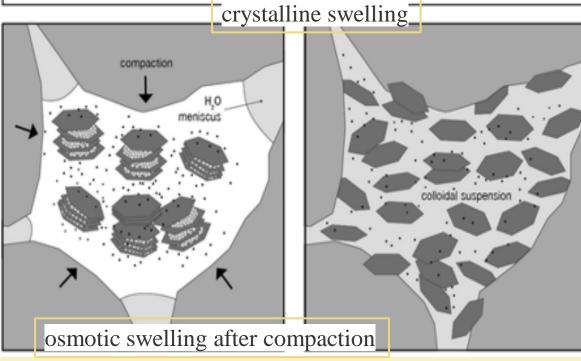


WATERPROOFING WITH CLAY

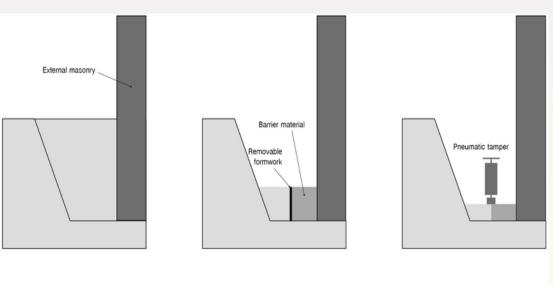


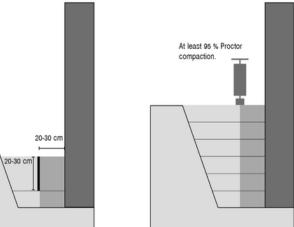


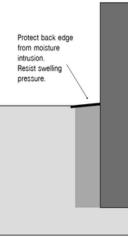




Properties that will contribute towards low hydraulic conductivity when a soil is compacted







Favourable grain distribution may result in a densely consolidated matrix

The presence of swelling clays can bind water during hydration.

A certain optimum moisture content will be necessary in order to achieve Proctor compaction (maximum density of consolidated grains)

The proportion of clay to silt and sand should not allow for shrinkage to form cracks in the compacted mass during dehydration

•
$$\rho_d = \frac{\rho_{Pr}}{(1 + \omega_{Pr}) * \rho_d}$$

•
$$\rho_d = \frac{\rho_{Pr}}{(1+\omega_{Pr})*\rho_d}$$
• $n = \left(1 - \frac{\rho_d}{\rho_s}\right)*100\%$

•
$$S = \frac{\left(\frac{\rho_d}{\rho_W * \omega_{Pr}}\right)}{\left(\frac{n}{100\%}\right)}$$

•
$$\omega_S = \left(\frac{V_d}{m_d} - \frac{1}{\rho_s}\right) * \rho_W$$

pd is the bulk density,

 ρ_{Pr} is the Proctor density,

 ρ_s is the measured particle density and

 ρ_w is the density of water in g/cm³;

 w_{Pr} is the optimum moisture content as a percentage of mass;

n is the total porosity as a percentage of total volume of the consolidated mass,

S is the degree of saturation as a percentage of total porosity.

 w_s is the moisture content at shrinkage limit as a percentage of total mass;

 V_d the volume of the dried sample in cm³;

 m_d the mass of the dried sample in g;

 ρs the particle density of the sample and ρw the density of water in g/cm³

THANK YOU FOR YOUR ATTENTION

